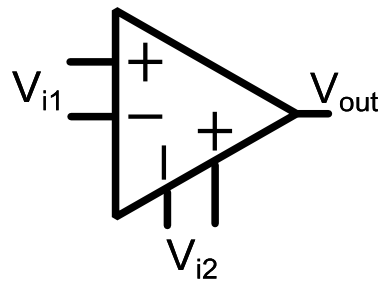


## Offset compensation using an additional input port

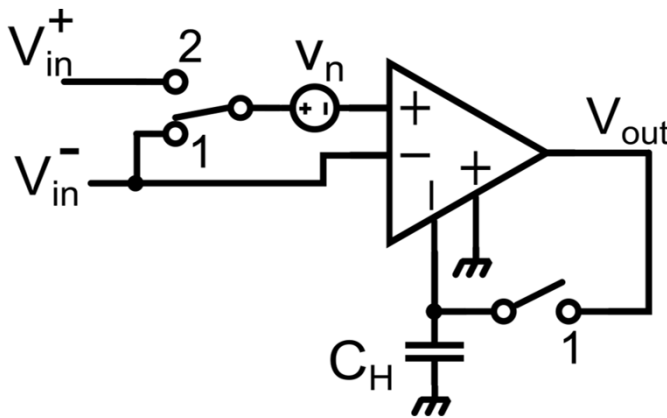


$$V_{out} = A(V_{i1} - v_n) + BV_{i2}$$

$V_{i1}$  is the input signal port,  $V_{i2}$  is the offset calibration port

(offset and noise are referred to the input signal port)

### AZ compensation:



Phase 1:

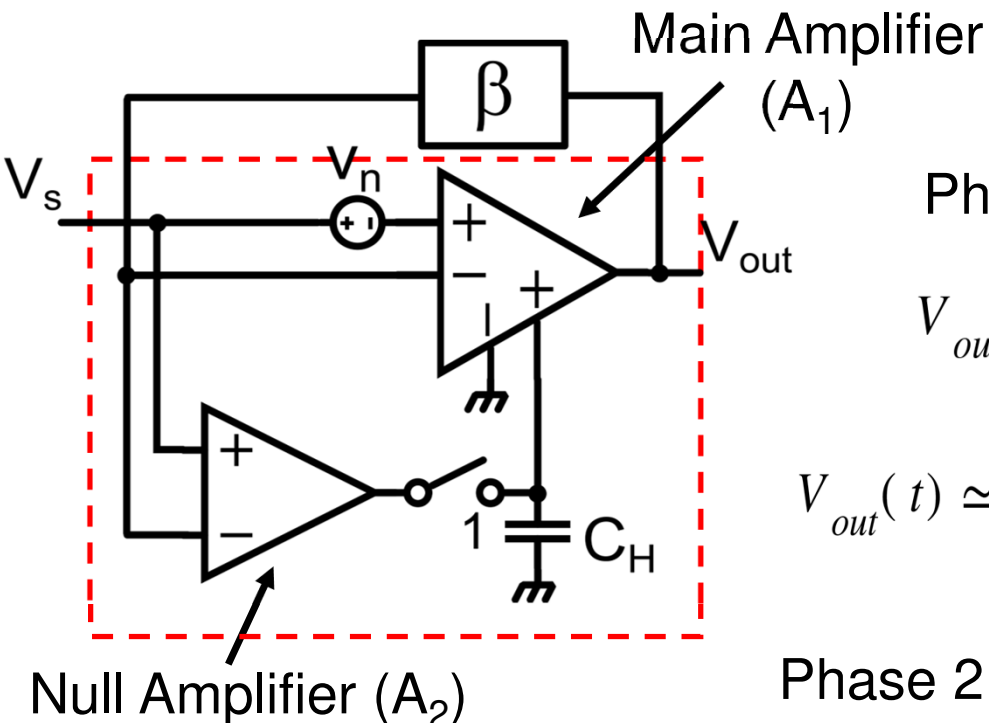
$$V_{out}(t) = -Av_n(t) - BV_{out}(t) \Rightarrow V_{out}(t) = -\frac{A}{1+B}v_n(t)$$

$$V_{C_H}(t) = V_{out}(t)$$

Phase 2:

$$V_{out}(t) = A(V_{in}^+(t) - V_{in}^-(t) - v_n(t)) - BV_{C_H}^{(1)} \Rightarrow V_{out}(t) \simeq A(V_{in}^+(t) - V_{in}^-(t) - \underbrace{(v_n(t) - v_n^{(1)})}_{v_{n-eff}(t)})$$

# Continuous-time AZ amplifiers



Hp.: Null Amplifier without offset

Phase 1:

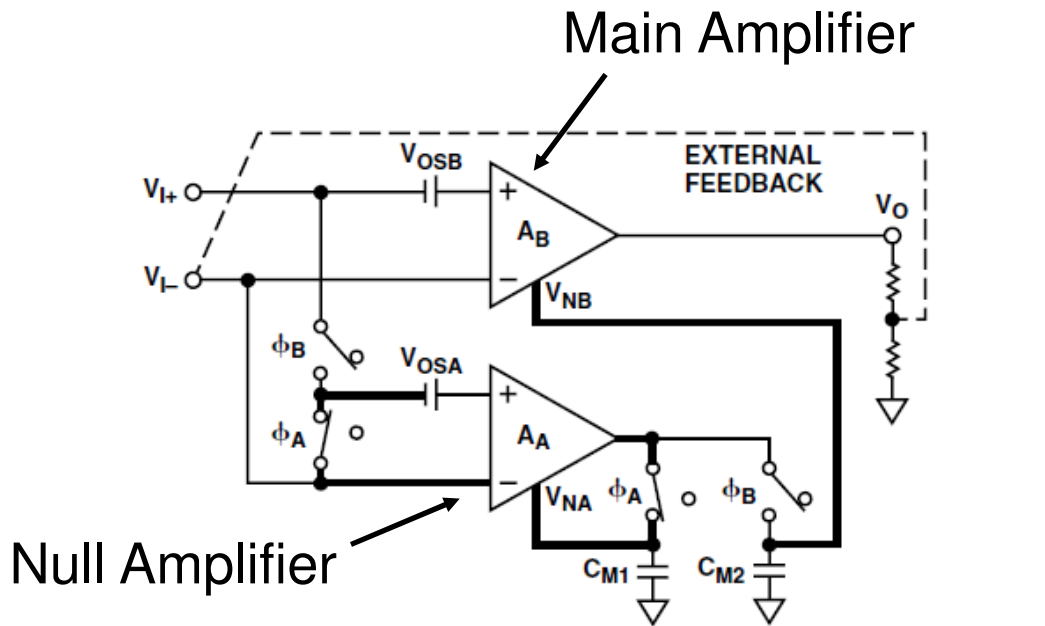
$$V_{out}(t) = A_1 (V_s - \beta V_{out} - v_n) + B_1 A_2 (V_s - \beta V_{out})$$

$$V_{out}(t) \simeq \frac{V_s}{\beta} - \frac{v_n A_1}{\beta (A_1 + B_1 A_2)} \quad \Rightarrow \quad v_{n-eff}(t) \simeq \frac{v_n(t) A_1}{B_1 A_2}$$

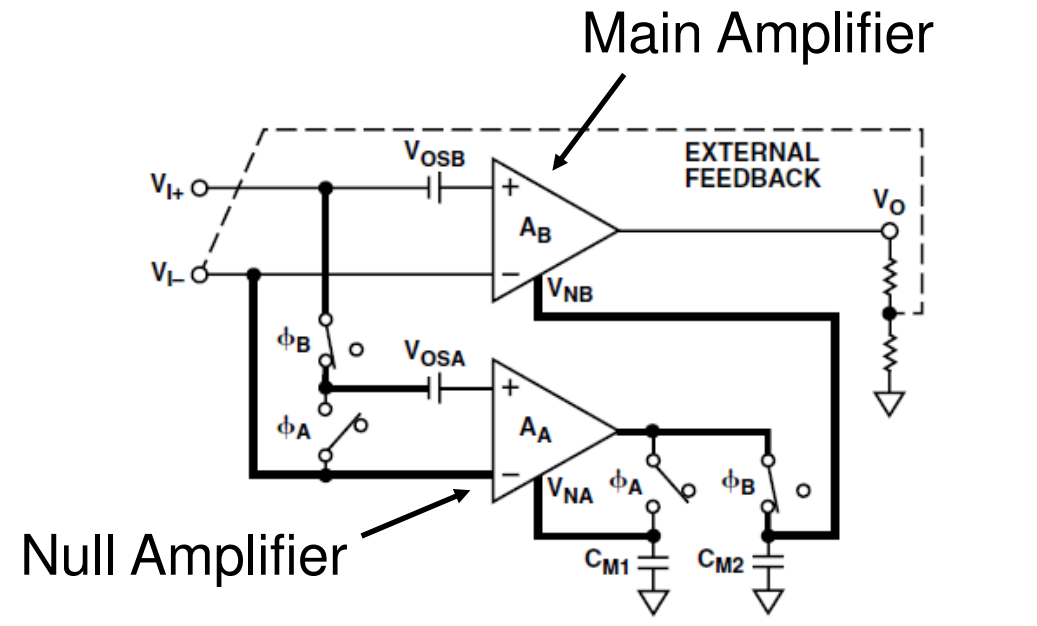
Phase 2:

$$V_{out}(t) = A_1 (V_s - \beta V_{out} - v_n) + B_1 A_2 V_{C_H}^{(1)} \quad \Rightarrow \quad V_{out}(t) \simeq \frac{V_s}{\beta} - A_1 \left( \overbrace{v_n(t) - v_n^{(1)}}^{v_{n-eff}(t)} \right)$$

## Commercial Zero-Drift Operational Amplifiers based on AZ (AD8551, TLC2654, OPA335...)

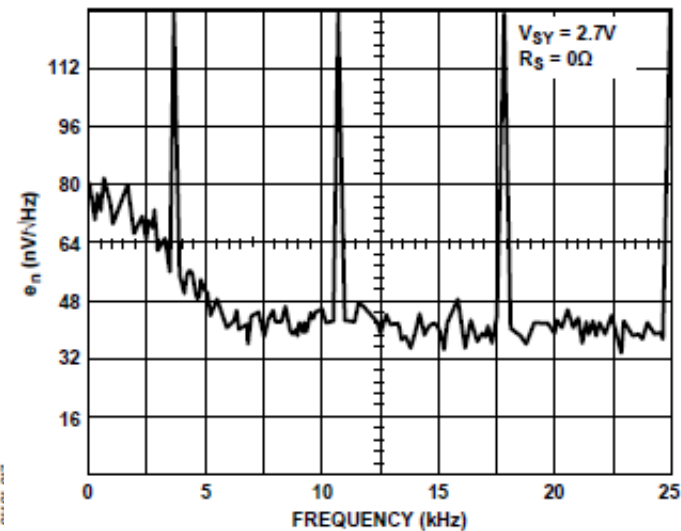
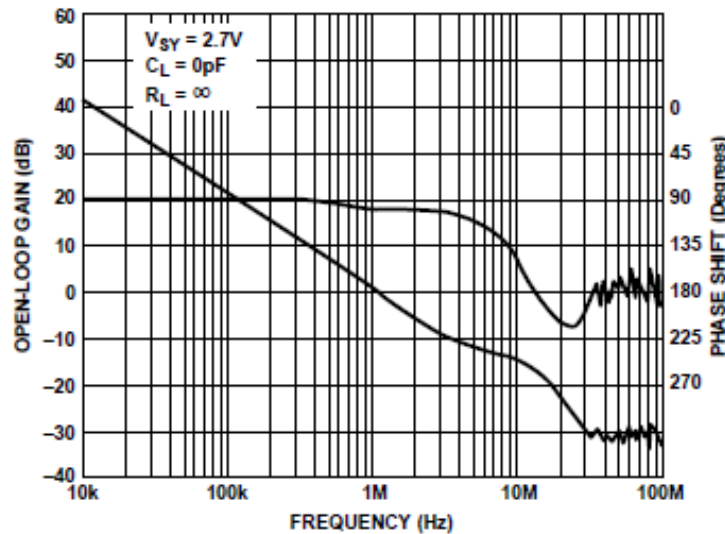
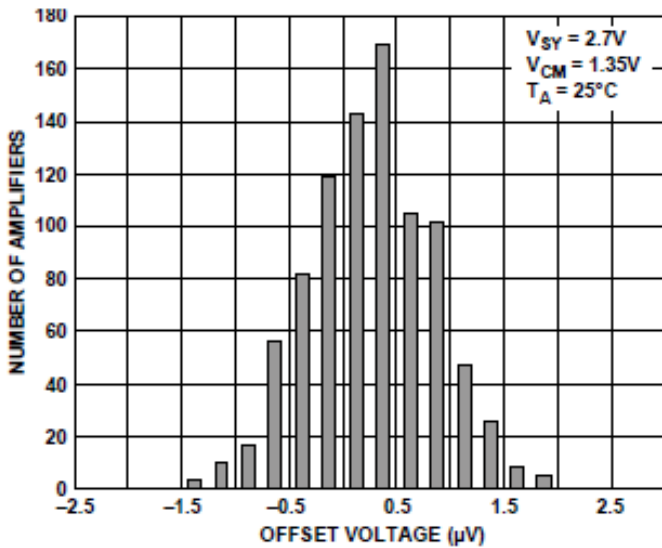


a. Auto-Zero Phase A: null amplifier nulls its own offset.



b. Output Phase B: null amplifier nulls the main amplifier offset.

# Commercial Zero-Drift Operational Amplifiers based on AZ (AD8551)

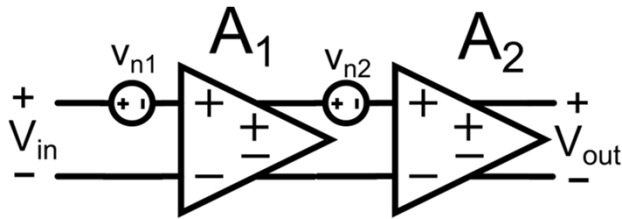


$$f_{\text{AZ}} = 4 \text{ kHz}$$

## Commercial Zero-Drift Operational Amplifiers based on AZ (AD8551, TLC2654, OPA335...)

Parameter	Symbol	Conditions	Min	Typ	Max	Unit
<b>POWER SUPPLY</b>						
Power Supply Rejection Ratio	PSRR	$V_S = 2.7\text{ V to } 5.5\text{ V}$ $-40^\circ\text{C} \leq T_A \leq +125^\circ\text{C}$	120	130		dB
Supply Current/Amplifier	$I_{SY}$	$V_O = 0\text{ V}$ $-40^\circ\text{C} \leq T_A \leq +125^\circ\text{C}$	115	130		dB
				850	975	$\mu\text{A}$
				1000	1075	$\mu\text{A}$
<b>DYNAMIC PERFORMANCE</b>						
Slew Rate	SR	$R_L = 10\text{ k}\Omega$		0.4		$\text{V}/\mu\text{s}$
Overload Recovery Time				0.05	0.3	ms
Gain Bandwidth Product	GBP			1.5		MHz
<b>NOISE PERFORMANCE</b>						
Voltage Noise	$e_n$ p-p	0 Hz to 10 Hz		1.0		$\mu\text{V p-p}$
	$e_n$ p-p	0 Hz to 1 Hz		0.32		$\mu\text{V p-p}$
Voltage Noise Density	$e_n$	$f = 1\text{ kHz}$		42		$\text{nV}/\sqrt{\text{Hz}}$
Current Noise Density	$i_n$	$f = 10\text{ Hz}$		2		$\text{fA}/\sqrt{\text{Hz}}$

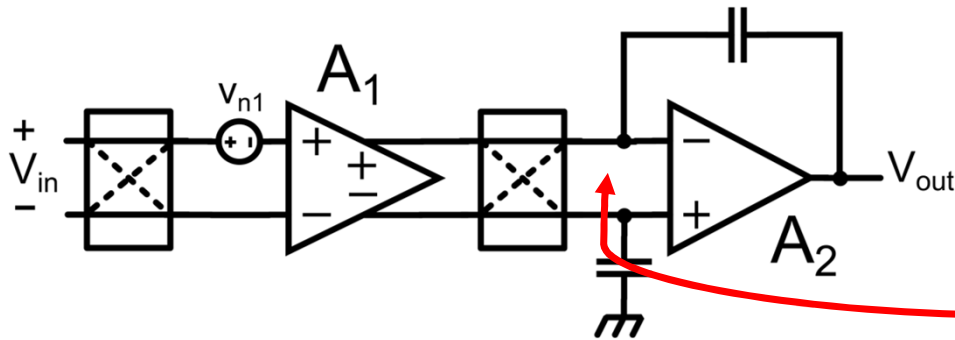
# Chopper Amplifier



$$v_{n-out} = A_1 A_2 v_{n1} + A_2 v_{n2}$$

$$v_{n-eff} = v_{n1} + \frac{v_{n2}}{A_1}$$

RTI offset of the second stage is attenuated by  $A_1$

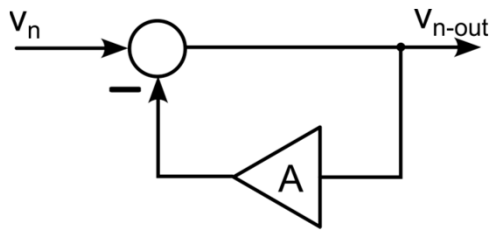


We can apply CHS only to the first stage and use the second stage as 1° order LPF (e.g. Miller Compensation)

Offset ripple is too large to be rejected by a 1° order LPF

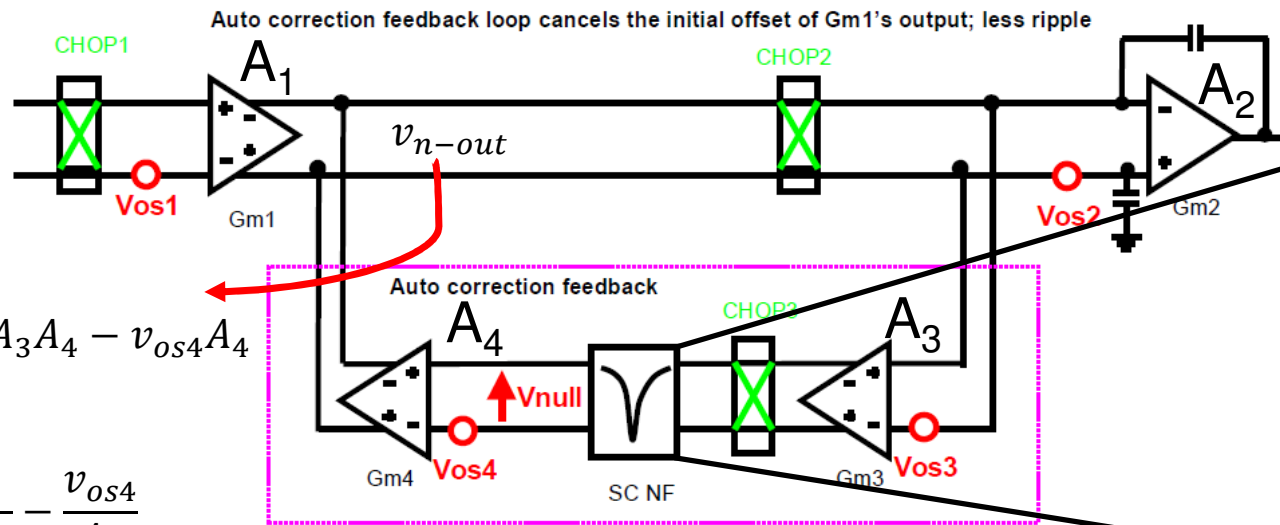
\* Y. Jusuda, "Auto Correction Feedback for Ripple Suppression in a Chopper Amplifier" – IEEE JSSC 2010

# Auto-Correction Feedback for Ripple Suppression\*

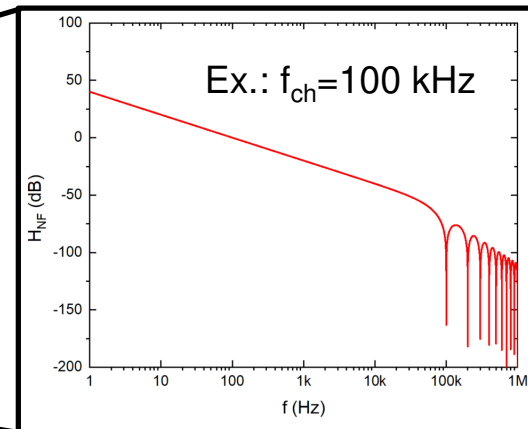


$$v_{n-out} = v_n - Av_{n-out} \quad \Rightarrow \quad v_{n-out} = \frac{v_n}{1 + A}$$

Amplifier A must be without offset and input signal must not be attenuated!



Auto correction feedback loop cancels the initial offset of Gm1's output; less ripple



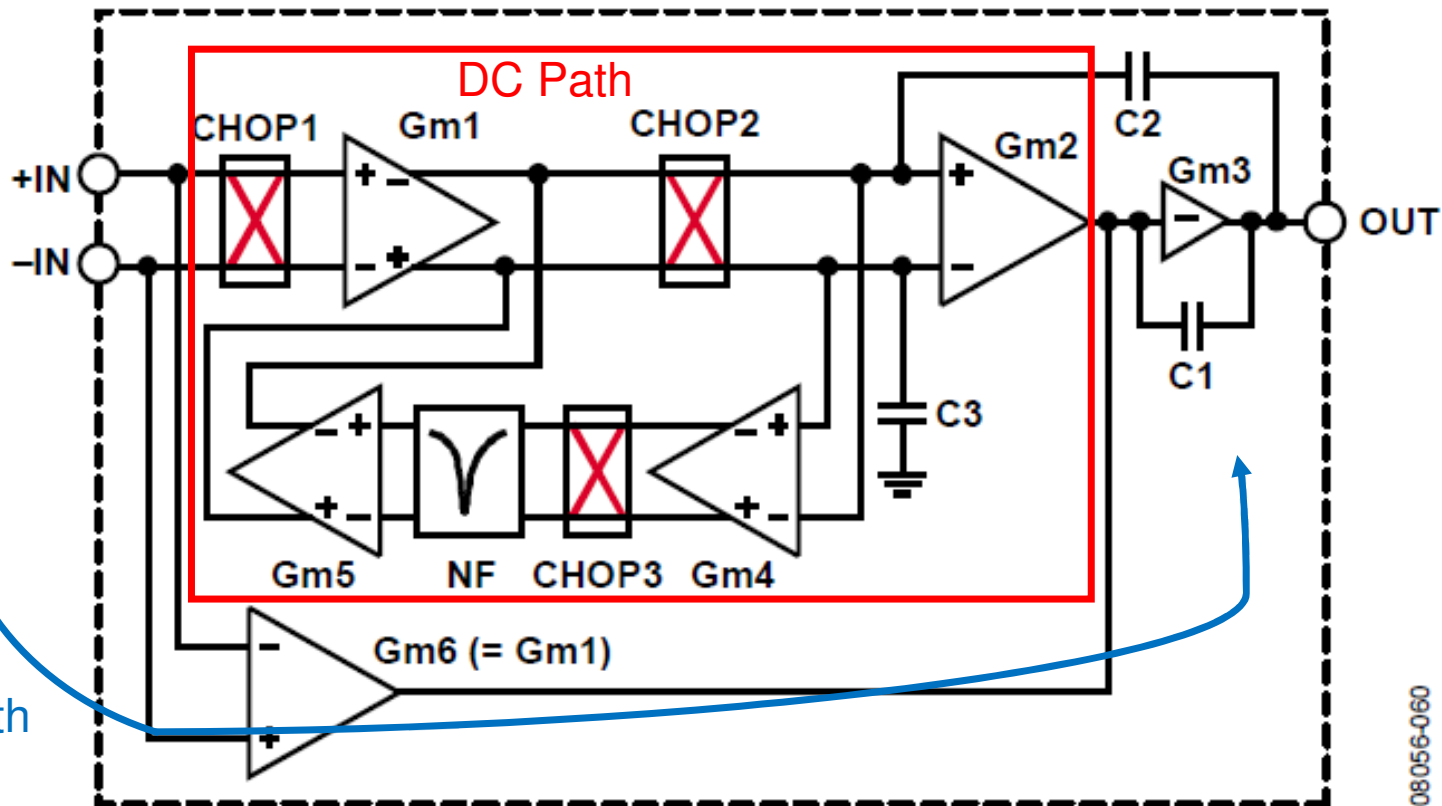
$$v_{n-out} = v_{os1}A_1 - v_{n-out}A_3A_4 - v_{os4}A_4$$

$$\Downarrow$$

$$v_{n-out} = \frac{v_{os1}A_1}{1 + A_3A_4} - \frac{v_{os4}}{A_3}$$

\* Y. Jusuda, "Auto Correction Feedback for Ripple Suppression in a Chopper Amplifier" – IEEE JSSC 2010

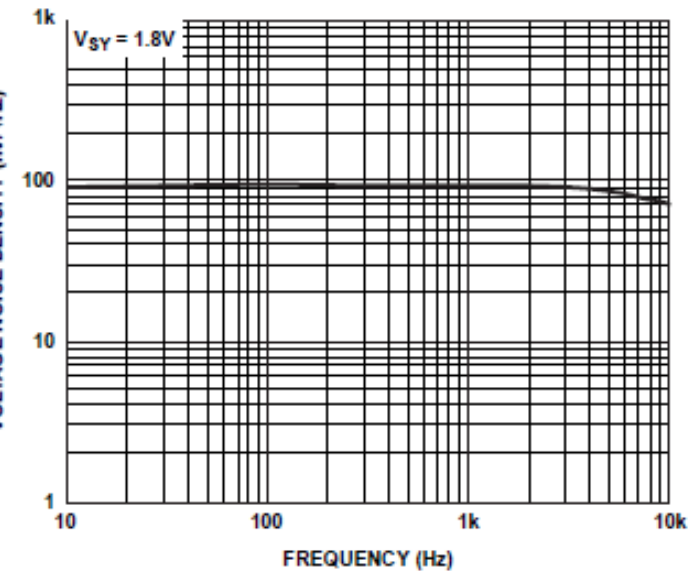
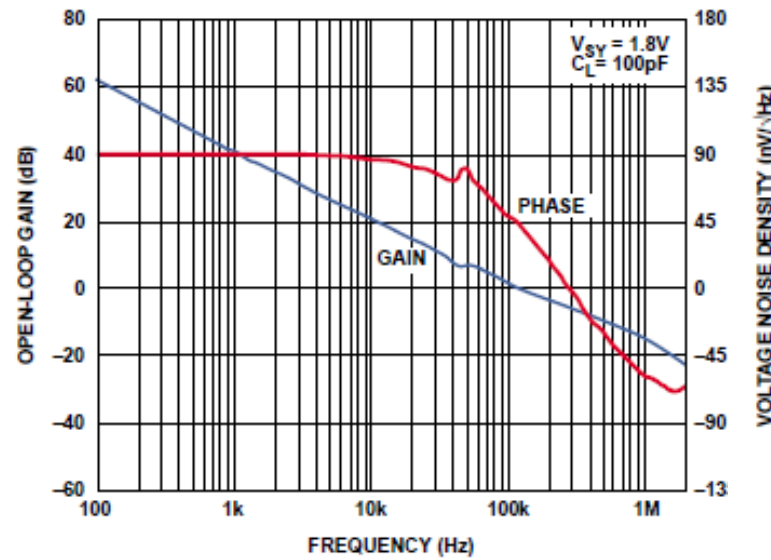
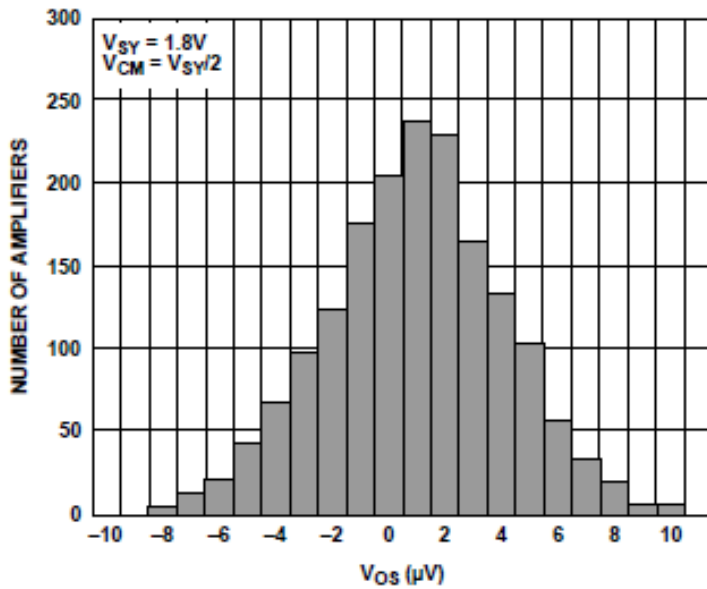
## Commercial Zero-Drift Operational Amplifiers based on CHS (ADA4051)



08056-060



# Commercial Zero-Drift Operational Amplifiers based on CHS (ADA4051)



$$f_{ch} = 40 \text{ kHz}$$

## Commercial Zero-Drift Operational Amplifiers based on CHS (ADA4051)

Parameter	Symbol	Test Conditions/Comments	Min	Typ	Max	Unit
<b>POWER SUPPLY</b>						
Power Supply Rejection Ratio	PSRR	$1.8\text{ V} \leq V_{SY} \leq 5.5\text{ V}$ $-40^\circ\text{C} \leq T_A \leq +125^\circ\text{C}$	110 106	135		dB dB
Supply Current per Amplifier	$I_{SY}$	$V_{OUT} = V_{SY}/2$		13	17	$\mu\text{A}$
ADA4051-2		$V_{OUT} = V_{SY}/2$		15	18	$\mu\text{A}$
ADA4051-1		$-40^\circ\text{C} \leq T_A \leq +125^\circ\text{C}$			20	$\mu\text{A}$
<b>DYNAMIC PERFORMANCE</b>						
Slew Rate	SR+	$R_L = 10\text{ k}\Omega, C_L = 100\text{ pF}, G = 1$		0.04		$\text{V}/\mu\text{s}$
	SR-	$R_L = 10\text{ k}\Omega, C_L = 100\text{ pF}, G = 1$		0.03		$\text{V}/\mu\text{s}$
Settling Time	$t_s$	To 0.1%, $V_{IN} = 1\text{ V p-p}$ , $R_L = 10\text{ k}\Omega, C_L = 100\text{ pF}$		120		$\mu\text{s}$
Gain Bandwidth Product	GBP	$C_L = 100\text{ pF}, G = 1$		115		kHz
Phase Margin	$\Phi_M$	$C_L = 100\text{ pF}, G = 1$		40		Degrees
Channel Separation	CS	$V_{IN} = 1.7\text{ V}, f = 100\text{ Hz}$		140		dB
<b>NOISE PERFORMANCE</b>						
Voltage Noise	$e_n$ p-p	$f = 0.1\text{ Hz to }10\text{ Hz}$		1.96		$\mu\text{V p-p}$
Voltage Noise Density	$e_n$	$f = 1\text{ kHz}$		95		$\text{nV}/\sqrt{\text{Hz}}$
Current Noise Density	$i_n$	$f = 1\text{ kHz}$		100		$\text{fA}/\sqrt{\text{Hz}}$