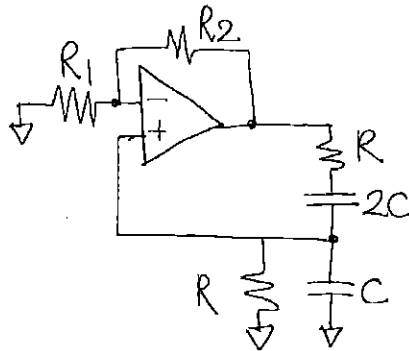


Prova scritta di Elettronica – Corso di Laurea in Ingegneria delle Telecomunicazioni

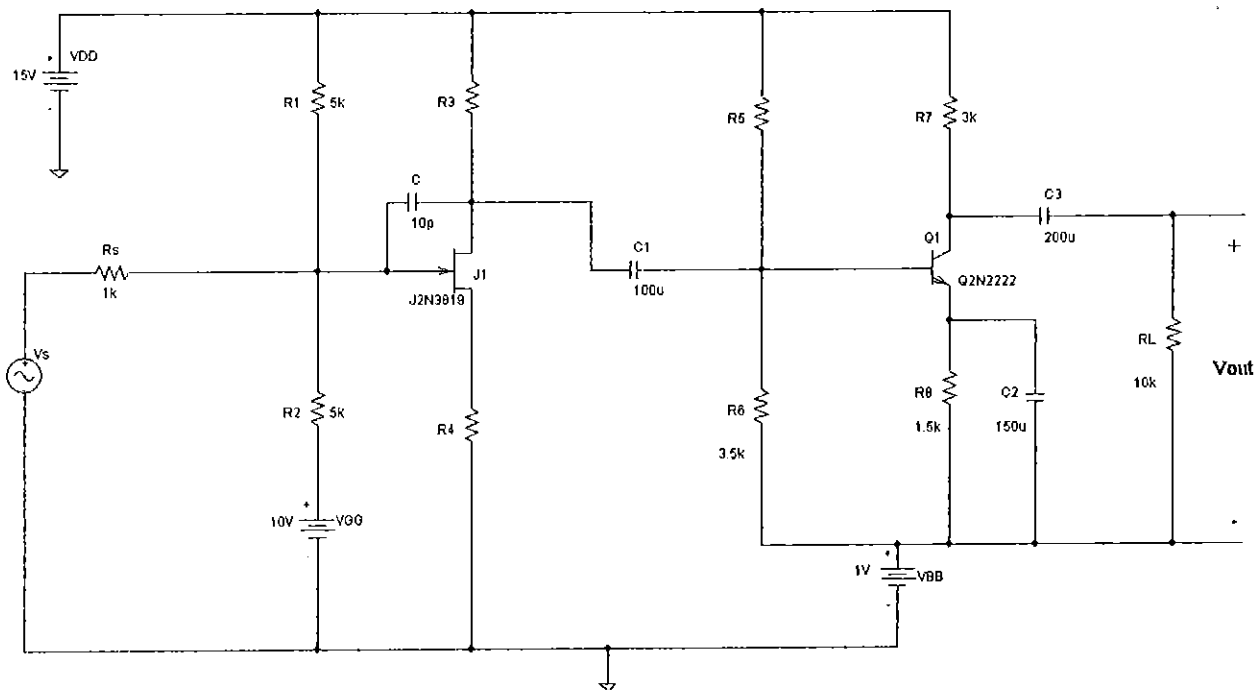
1 Febbraio 2012

- Si consideri un amplificatore con amplificazione di tensione in continua $A_{v0}=5000$, $R_{in} = 130 \text{ K}\Omega$, $R_{out} = 2 \text{ K}\Omega$, un polo a frequenza $f_p = 300 \text{ Hz}$. Inoltre sia $R_s = 2 \text{ K}\Omega$ la resistenza del generatore di segnale e $R_L = 200 \Omega$ la resistenza del carico. Si reazioni il circuito in modo da ottenere una resistenza di ingresso maggiore di $2 \text{ M}\Omega$ e una resistenza di uscita di $1 \text{ M}\Omega$. (con una tolleranza del 5%)
- Sia dato l'oscillatore a lato. Verificare il criterio di Barkhausen all'innesco e calcolare l'eventuale frequenza di oscillazione. Sia $R=1 \text{ K}\Omega$, $C = 50 \text{ nF}$, $R_1=10 \text{ K}\Omega$, $R_2=15 \text{ K}\Omega$.



- Dato l'amplificatore disegnato in figura, calcolare:
 - I valori delle resistenze R_3, R_4, R_5 sapendo che: $I_{DS} = 1.8 \text{ mA}$, $V_{DS} = 6.9 \text{ V}$ e che $I_C = 2.7 \text{ mA}$ (Punteggio 5/30)
 - l'amplificazione V_u/V_s a centrobanda (Punteggio 4/30)
 - il limite superiore di banda e il limite inferiore di banda (Punteggio 8/30)

NOTE: J1 è un 2N3819 con $r_d \rightarrow \infty$, Q1 un QN2222 con $h_{oe} = 0$.

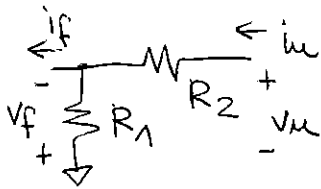
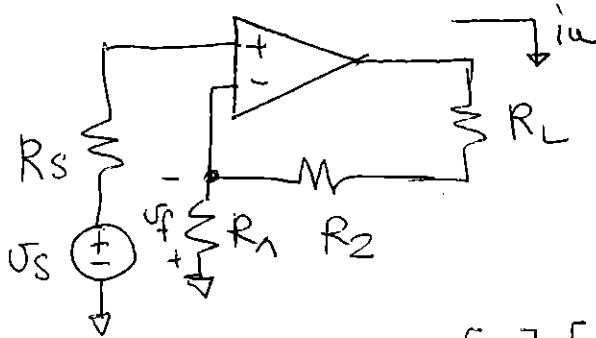


Es. 1.

$R_{in} = 130 \text{ k}\Omega \rightarrow R_{IF} > 2 \text{ M}\Omega$

$R_{out} = 2 \text{ k}\Omega \rightarrow R_{OF} = 1 \text{ M}\Omega$

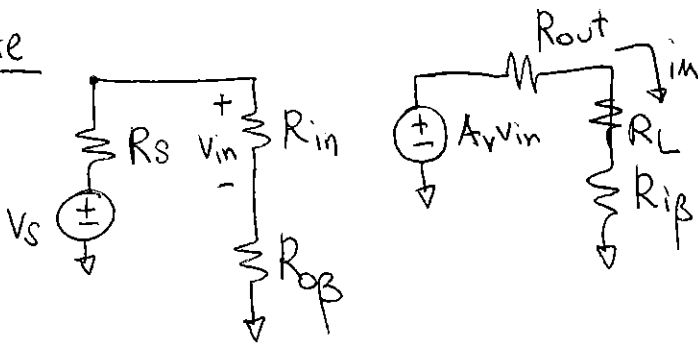
È necessaria una reazione con inserzione di tensione e prelievo di corrente



$$\begin{bmatrix} v_f \\ v_m \end{bmatrix} = \begin{bmatrix} \beta & R_{o\beta} \\ R_{i\beta} & K \end{bmatrix} \begin{bmatrix} i_u \\ i_f \end{bmatrix}$$

$\beta = \frac{v_f}{i_u} \Big|_{i_f=0} = -R_1$; $R_{o\beta} = \frac{v_f}{i_f} \Big|_{i_u=0} = R_1$; $R_{i\beta} = \frac{v_m}{i_m} \Big|_{i_f=0} = R_1 + R_2$

A_e



$$A_e = \frac{i_m}{v_s} \Big|_{\beta=0} = \frac{R_{in}}{R_{in} + R_s + R_{o\beta}} \cdot A_v \frac{1}{R_{out} + R_{i\beta}}$$

$$A_e = \frac{R_{in}}{R_{in} + R_s + R_1} A_v \frac{1}{R_{out} + R_1 + R_2 + R_L}$$

$$R_{OF} = (R_{out} + R_{i\beta}) \Big|_{R_L=0} (1 - \beta A_e) = \underset{2 \text{ k}\Omega}{(R_{out} + R_{i\beta})} \left[1 + \frac{R_{in}}{R_{in} + R_s + R_{o\beta}} \overset{R_1 + R_2}{A_v} \frac{R_1}{R_{out} + R_{i\beta}} \right] \overset{5000}{}$$

Per avere $R_{OF} = 1 \text{ M}\Omega$ dobbiamo avere $|\beta A_e| \gg 1$, possiamo quindi trascurare 1 rispetto a βA_e :

$$R_{OF} = \frac{A_v R_{in} R_1}{R_{in} + R_s + R_1} \rightarrow R_1 = \frac{R_{in} + R_s}{\frac{A_v R_{in}}{R_{OF}} - 1} \approx \underline{203 \Omega}$$

$$R_{IF} = (R_{in} + R_{of}) \left(1 - \beta A_e \Big|_{R_s=0} \right) =$$

$$= (R_{in} + R_{of}) \left(1 + \frac{R_1 R_{in} A_v}{(R_{in} + R_{of})(R_{out} + R_1 \beta)} \right)$$

di nuovo trascuriamo 1, scegliamo $R_{IF} = 5 M\Omega$, e calcoliamo R_2

$$R_{IF} \approx \frac{R_1 R_{in} A_v}{R_{out} + R_1 + R_2} \rightarrow R_2 = \frac{R_1 R_{in} A_v}{R_{IF}} - R_{out} - R_1$$

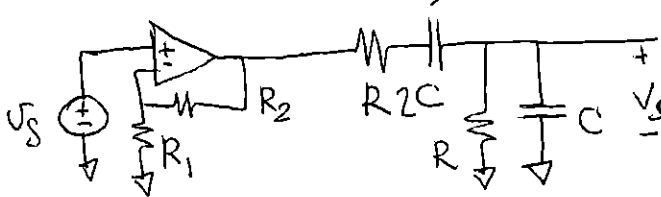
$$= 24187$$

Sostituendo otteniamo:

$$R_{OF} = 1,026 M\Omega$$

$$R_{IF} = 5,14 M\Omega$$

2) ~~Apriamo l'anello di reazione~~ Apriamo l'anello di reazione:



$$\frac{V_s'}{V_s} = \frac{\frac{R}{1+RCs}}{\frac{R}{1+RCs} + R + \frac{1}{2Cs}} \cdot \left(1 + \frac{R_2}{R_1} \right) =$$

$$\beta A = \frac{V_s'}{V_s} = \frac{2RCs}{2RCs + 2RCs(1+RCs) + (1+RCs)} \left(1 + \frac{R_2}{R_1} \right) =$$

$$\beta A = \frac{2RCs}{2RCs^2 + 5RCs + 1} \left(1 + \frac{R_2}{R_1} \right)$$

la fase è nulla se $1 - 2RC^2 \omega_0^2 \rightarrow \omega_0 = \frac{1}{\sqrt{2} RC} = \frac{1}{1,41 \cdot 1000 \cdot 50 \cdot 10^{-9}} =$

$$\omega_0 = 14,18 \text{ Krad/s}$$

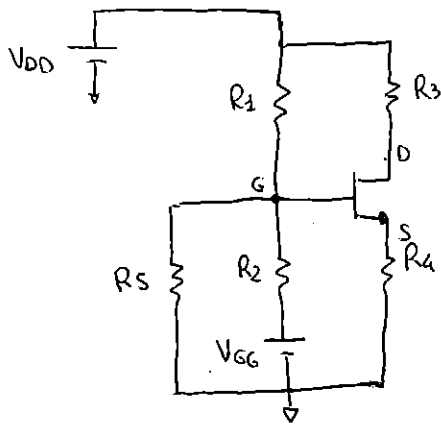
$$\beta A(\omega_0) = \frac{2}{5} \left(1 + \frac{15}{10} \right) = 1$$

al limite dell'inescus NON si può dire se l'oscillazione si innesca.

LA CAPACITA' C HA UN VALORE DELL'ORDINE DEI pF, QUINDI COMPARABILE CON LE CAPACITA' INTRINSECHE DEL JFET E DEL BJT. L'UNICO EFFETTO CHE HA E' DI FINIRE IN PARALLELO A C_{GD} , QUINDI E' COME SE AVESSIMO UN JFET CON UNA

$$C'_{GD} = C_{GD} + C$$

PUNTO DI RIPOSO JFET



HP. JFET IN SATURAZIONE

PRINCIPIO DI SOVRAPPOSIZIONE DEGLI EFFETTI

$$V_G = V_{GG} \cdot \frac{R_1 // R_5}{R_1 // R_5 + R_2} + V_{DD} \cdot \frac{R_2 // R_5}{R_2 // R_5 + R_1} \cong 3.5V$$

$$V_{GS} = V_G - V_S$$

$$V_{GS} = V_G - R_4 \cdot I_{DS}$$

$$I_{DS} = \frac{V_G - V_{GS}}{R_4}$$

DALLE CARATTERISTICHE VEDO CHE PER $T=25^\circ C$ PER $I_{DS} = 1.8mA$ RISULTA $V_{GS} \cong -1.9V$

$$R_4 = \frac{V_G - V_{GS}}{I_{DS}} \cong 3k\Omega$$

$$R_4 = 3k\Omega$$

$$V_{DS} = V_{DD} - (R_3 + R_4) I_{DS}$$

$$R_3 + R_4 = \frac{V_{DD} - V_{DS}}{I_{DS}} \cong 4.5k\Omega$$

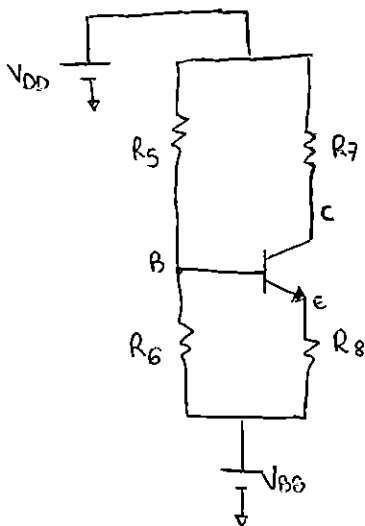
$$R_3 = 4.5k\Omega - R_4 \cong 1.5k\Omega$$

$$R_3 = 1.5k\Omega$$

VERIFICA HP. JFET IN SATURAZIONE

$$\begin{cases} V_{GS} > V_p & -1.9V > -3V \text{ ok!} \\ V_{DS} > V_{GS} - V_p & 6.9V > (-1.9 + 3)V \text{ ok!} \end{cases}$$

PUNTO DI RIPOSO BJT



HP. PARTITORE PESANTE.

PRINCIPIO DI SOVRAPPOSIZIONE DEGLI EFFETTI

$$V_B = V_{BB} \cdot \frac{R_5}{R_5 + R_6} + V_{DD} \cdot \frac{R_6}{R_5 + R_6} \quad (*)$$

$$V_{BE} = V_B - V_E = V_{BE} \approx 0.7V$$

$$I_C \approx I_E = \frac{V_E - V_{BB}}{R_8}$$

$$V_E = V_{BB} + R_8 \cdot I_C \approx 5.05V$$

$$V_B = V_E + V_{BE} = 5.05V + 0.7V = 5.75V$$

Da (*) si ha:

$$V_B \cdot (R_5 + R_6) = V_{BB} \cdot R_5 + V_{DD} \cdot R_6$$

$$(V_B - V_{BE}) R_S = (V_{DD} - V_B) R_G$$

$$R_S = \frac{(V_{DD} - V_B)}{(V_B - V_{BE})} \cdot R_G = \frac{15 - 5.75}{5.75 - 1} \cdot 3.5 \text{ k}\Omega \approx 7 \text{ k}\Omega$$

$$R_S = 7 \text{ k}\Omega$$

$$V_C = V_{DD} - R_7 \cdot I_C \approx 6.9 \text{ V}$$

$$V_{CE} = V_C - V_E \approx 1.85 \text{ V}$$

VERIFICA HP. PARTITORE PESANTE

$$h_{FE} \approx 160$$

$$I_B = \frac{I_C}{h_{FE}} \approx 16.9 \mu\text{A}$$

$$I_{RS} = \frac{V_{DD} - V_B}{R_S} \approx 1.33 \mu\text{A}$$

$$I_{RG} = \frac{V_B - V_{BE}}{R_G} \approx 1.33 \mu\text{A}$$

$$I_B \ll I_{RS}, I_{RG}$$

PARAMETRI DI PICCOLO SEGNALE

• JFET

$$g_m \approx 2.7 \text{ mS} \quad (\text{letta per } V_{GS} \approx -1.9 \text{ V})$$

$$C_{iss} \approx 2 \text{ pF} \quad (\text{letta sulla curva } V_{DS} = 10 \text{ V})$$

$$C_{rss} \approx 0.9 \text{ pF}$$

$$C_{GD} = C_{rss} = 0.9 \text{ pF} \rightarrow C_{GD}' = C_{GD} + C = 10.9 \text{ pF}$$

$$C_{GS} = C_{iss} - C_{rss} = 1.1 \text{ pF}$$

• BJT

$$R_{\beta} = \frac{50 + 300}{2} = 175$$

$$r_{ie} @ 1 \text{ mA} = \frac{2 + 8}{2} = 5 \text{ k}\Omega$$

$$V_{be} @ 1 \text{ mA} = \frac{V_T \cdot R_{\beta}}{I_C @ 1 \text{ mA}} = 4.55 \text{ k}\Omega$$

$$V_{bb'} = R_{ie} - V_{b'e} = 450.2$$

$$V_{b'e} = \frac{V_T \cdot \beta \beta_e}{I_C} \approx 1.69 \text{ k}\Omega$$

$$R_{ie} = V_{b'e} + V_{bb'} = 2.14 \text{ k}\Omega$$

$$V_{CB} = V_{CE} - V_{BE} = 1.15 \text{ V}$$

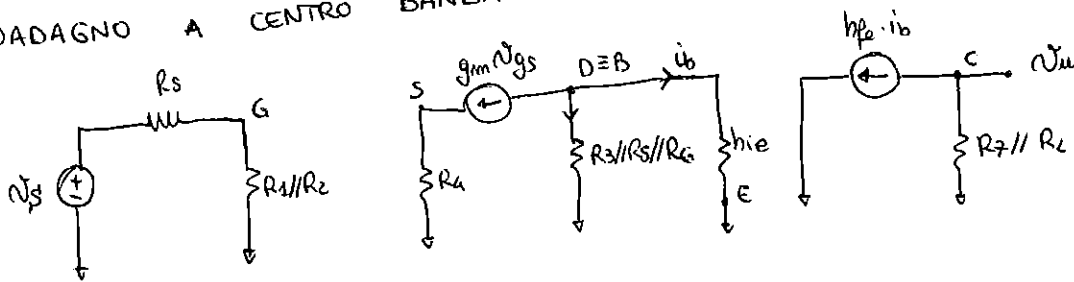
$$f_T \approx 160 \text{ MHz}$$

$$g_{m_{BJT}} = \frac{I_C}{V_T} \approx 103.85 \text{ mS}$$

$$C_{b'c} \approx 7 \text{ pF}$$

$$C_{b'e} = \frac{g_{m_{BJT}}}{2\pi f_T} - C_{b'c} \approx 96.3 \text{ pF}$$

GUADAGNO A CENTRO BANDA



$$V_u = -R_L // R_7 \beta \beta_e \cdot i_b$$

$$i_b = -g_m N_s - \frac{V_u}{R_3 // R_5 // R_6} = -g_m N_s - \frac{h_{fe} \cdot i_b}{R_3 // R_5 // R_6}$$

$$i_b \left(1 + \frac{h_{fe}}{R_3 // R_5 // R_6} \right) = -g_m N_s$$

$$i_b = \frac{-g_m N_s (R_3 // R_5 // R_6)}{h_{fe} + (R_3 // R_5 // R_6)}$$

$$N_s = N_g - N_s$$

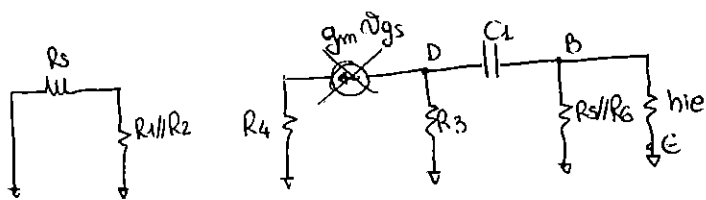
$$\tilde{V}_{gs} = \tilde{V}_s \frac{R_1 // R_2}{R_1 // R_2 + R_s} - R_4 g_m \tilde{V}_{gs}$$

$$\tilde{V}_{gs} = \frac{\frac{R_1 // R_2}{R_1 // R_2 + R_s} \cdot \tilde{V}_s}{1 + R_4 g_m} = \frac{R_1 // R_2}{R_1 // R_2 + R_s} \cdot \frac{1}{1 + R_4 g_m} \cdot \tilde{V}_s$$

$$i_b = -\frac{g_m (R_3 // R_5 // R_6)}{h_{ie} + (R_3 // R_5 // R_6)} \cdot \frac{R_1 // R_2}{R_1 // R_2 + R_s} \cdot \frac{1}{1 + R_4 g_m} \cdot \tilde{V}_s$$

$$A_{CB} = \frac{\tilde{V}_u}{\tilde{V}_s} = (R_L // R_7) h_{fe} \cdot \frac{g_m (R_3 // R_5 // R_6)}{h_{ie} + (R_3 // R_5 // R_6)} \cdot \frac{R_1 // R_2}{R_1 // R_2 + R_s} \cdot \frac{1}{1 + R_4 g_m} \approx 26$$

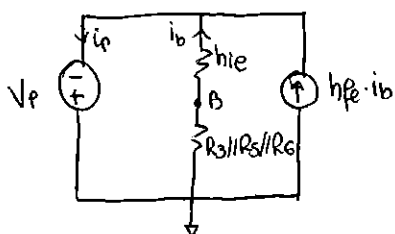
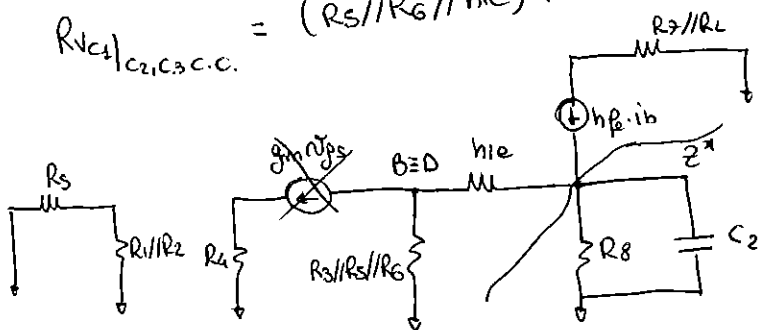
LIMITI INFERIORE DI BANDE



$$\tilde{V}_g = 0$$

$$\tilde{V}_s = 0$$

$$R_{V_{C1}, C_2, C_3, C_4} = (R_s // R_6 // h_{ie}) + R_3 \approx 2.62 \text{ K}\Omega$$

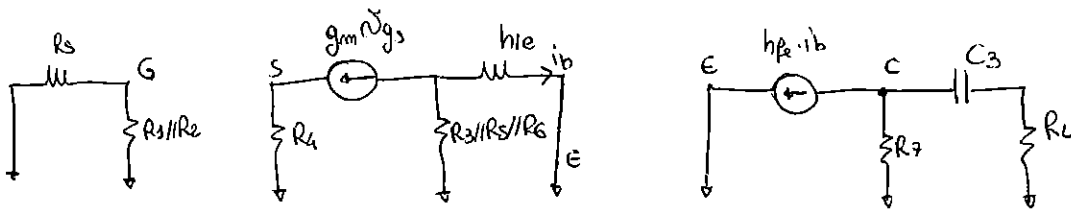


$$i_p = i_b + h_{fe} \cdot i_b = (1 + h_{fe}) \cdot i_b$$

$$V_p = (h_{ie} + R_3 // R_5 // R_6) \cdot i_b$$

$$Z^* = \frac{V_p}{i_p} = \frac{h_{ie} + R_3 // R_5 // R_6}{1 + h_{fe}} \approx 17.35 \Omega$$

$$R_{Vc2}|_{c1, c3 \text{ c.c.}} = R_8 // Z^* \cong 17.15 \Omega$$



$$\dot{N}_g = 0$$

$$\dot{N}_s = 0$$

$$i_b = 0$$

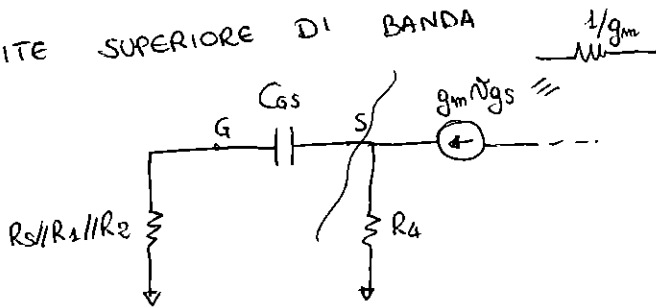
$$h_{fe} \cdot i_b = 0$$

$$R_{Vc3}|_{c1, c2 \text{ c.c.}} = R_7 + R_L = 13 \text{ k}\Omega$$

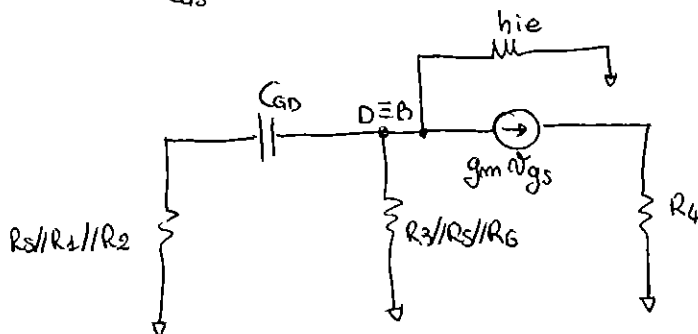
$$f_L = \frac{1}{2\pi} \left[\frac{1}{C_1 \cdot R_{Vc1}} + \frac{1}{C_2 \cdot R_{Vc2}} + \frac{1}{C_3 \cdot R_{Vc3}} \right] =$$

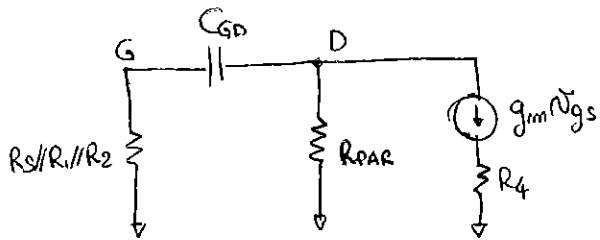
$$= \frac{1}{2\pi} \left[\frac{1}{100 \times 10^{-6} \times 2.62 \times 10^3} + \frac{1}{200 \times 10^{-6} \times 17.15} + \frac{1}{200 \times 10^{-6} \times 13 \times 10^3} \right] \cong 67 \text{ Hz}$$

LIMITE SUPERIORE DI BANDA



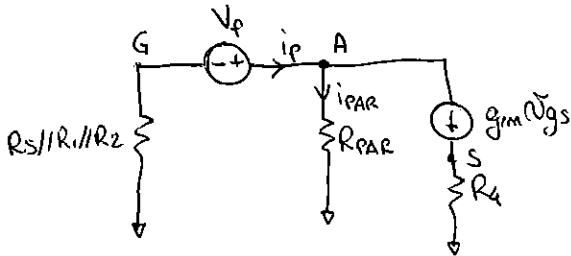
$$R_{Vgs} = (R_3 // R_1 // R_2) + \left(R_4 // \frac{1}{g_m} \right) \cong 330 \Omega$$





$$R_{PAR} = R_3 // R_5 // R_6 // h_{ie} \cong 640 \Omega$$

$$R_s // R_1 // R_2 \cong 714 \Omega$$



$$V_p = R_{PAR} \cdot i_{PAR} + (R_s // R_1 // R_2) \cdot i_p$$

$$i_p = i_{PAR} + g_m \tilde{V}_{gs}$$

$$\tilde{V}_{gs} = \tilde{V}_g - \tilde{V}_s = -(R_s // R_1 // R_2) \cdot i_p - R_4 g_m \tilde{V}_{gs}$$

$$\tilde{V}_{gs} = \frac{-(R_s // R_1 // R_2)}{1 + R_4 g_m} \cdot i_p$$

$$i_p = i_{PAR} - \frac{g_m (R_s // R_1 // R_2)}{1 + R_4 g_m} \cdot i_p$$

$$i_{PAR} = \frac{V_A}{R_{PAR}} = \frac{V_p - (R_s // R_1 // R_2) i_p}{R_{PAR}}$$

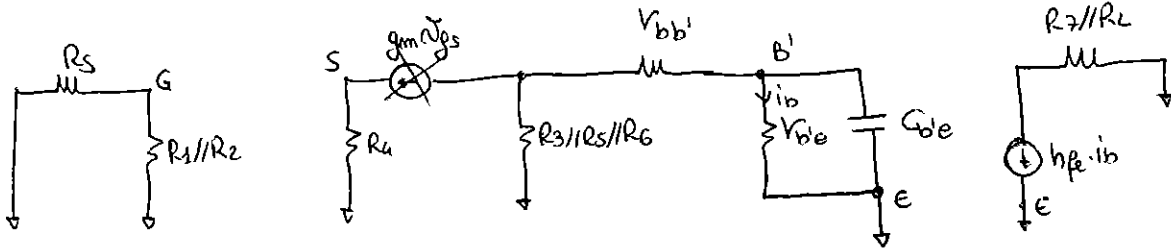
$$i_p = \frac{V_p}{R_{PAR}} - \frac{(R_s // R_1 // R_2)}{R_{PAR}} \cdot i_p - \frac{g_m (R_s // R_1 // R_2)}{1 + R_4 g_m} \cdot i_p$$

$$\left[1 + \frac{(R_s // R_1 // R_2)}{R_{PAR}} + \frac{g_m (R_s // R_1 // R_2)}{1 + R_4 g_m} \right] i_p = \frac{V_p}{R_{PAR}}$$

$$R_{V_{C_{GD}}} = \frac{V_p}{i_p} = R_{PAR} \left[1 + \frac{(R_S // R_1 // R_2)}{R_{PAR}} + \frac{g_m (R_S // R_1 // R_2)}{1 + R_4 g_m} \right] =$$

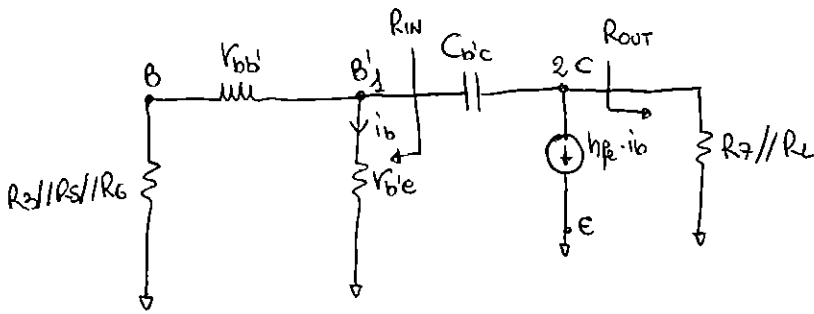
$$= R_{PAR} + (R_S // R_1 // R_2) + \frac{g_m (R_S // R_1 // R_2) \cdot R_{PAR}}{1 + R_4 g_m} =$$

$$= 640 + 714 + \frac{2.7 \times 10^{-3} \times 714 \times 640}{1 + 3 \times 2.7} \approx 1.5 \text{ k}\Omega$$



$$V_g = 0 \quad V_s = 0$$

$$R_{V_{C_{B'E}}} = V_{be} // (R_3 // R_S // R_G + V_{bb'}) \approx 754 \Omega$$



$$R_{IN} = R_{V_{C_{B'E}}} \approx 754 \Omega$$

$$R_{OUT} = R_7 // R_L \approx 2.31 \text{ k}\Omega$$

$$A_v = \frac{V_2}{V_1}$$

$$V_1 = V_{be} \cdot i_b$$

$$V_2 = -(R_7 // R_L) \cdot h_{fe} \cdot i_b$$

$$A_v = \frac{V_2}{V_1} = -\frac{(R_2/R_L)h_{\beta}}{r_{b'e}} \approx -239.2$$

$$R_{V_{C_{b'c}}} = R_{IN}(1+|A_v|) + R_{OUT} \approx 0.754(1+239.2) + 2.31 \approx 183.4 \text{ k}\Omega$$

$$f_H = \frac{1}{2\pi \left[C_{GS} \cdot R_{V_{C_{GS}}} + \underbrace{C_{GD}'}_{\parallel C_{GD}+C} \cdot R_{V_{C_{GD}}} + C_{b'e} \cdot R_{V_{C_{b'e}}} + C_{b'c} \cdot R_{V_{C_{b'c}}} \right]}$$

$$= \frac{1}{2\pi \left[1.1 \times 0.33 + 10.9 \times 1.5 + 96.3 \times 0.754 + 7 \times 183.4 \right] \times 10^{-9}} \approx 116 \text{ kHz}$$